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# **Adaptive Back Sheet Material for Acoustic Liner Application**

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NASA Aeronautics Research Mission Directorate (ARMD)

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# Outline

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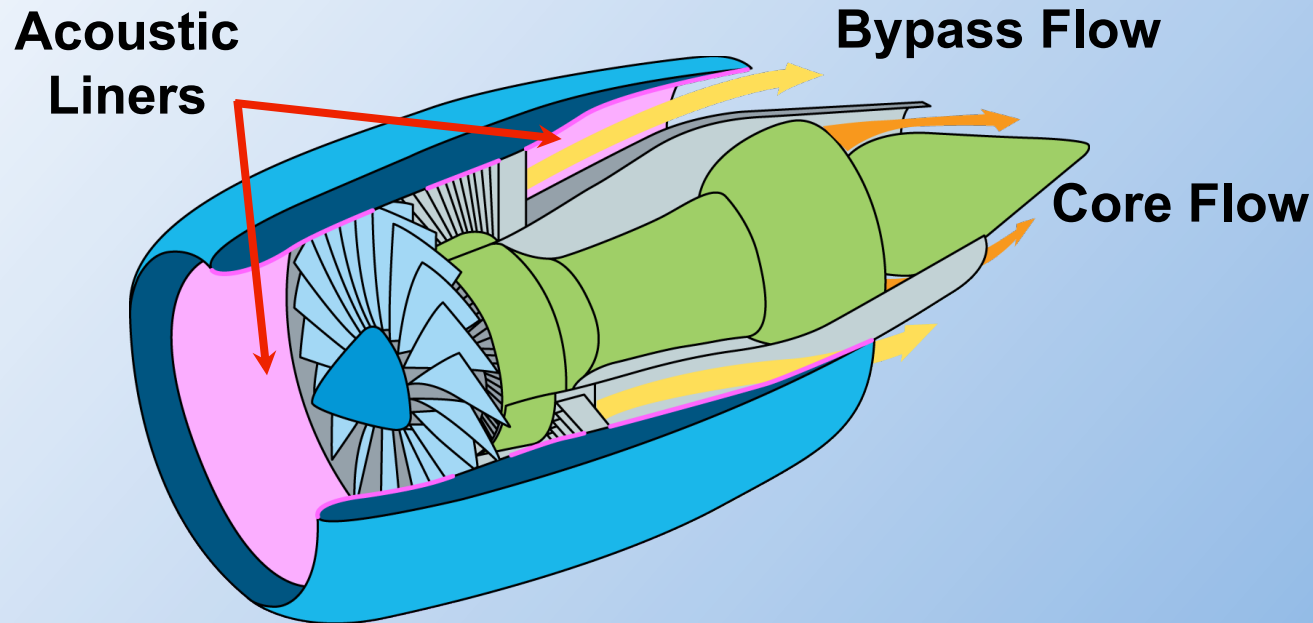
- Background
- Description of Piezo-electric Composite
- Results to Date
  - Mechanical
  - Acoustic
  - Lessons Learned
- Summary and Conclusions
- Next Steps



# The Challenge

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## Aircraft Engine Nacelle

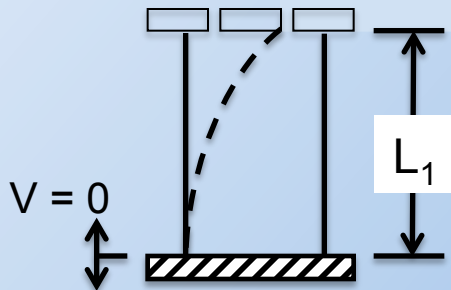
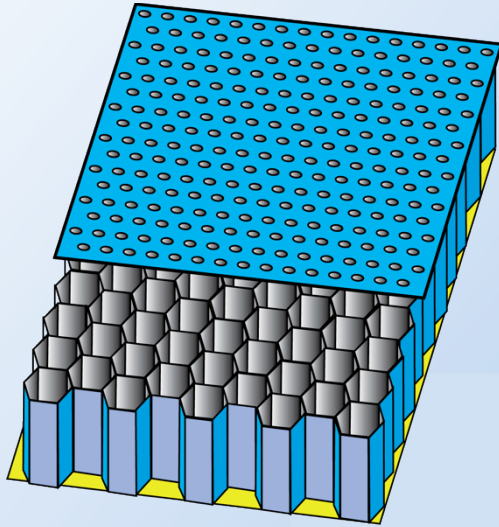


- Engine size increases
  - Frequency of source decreases
  - Nacelle treatment area decreases
- => Need to get more performance out of less acoustic liner

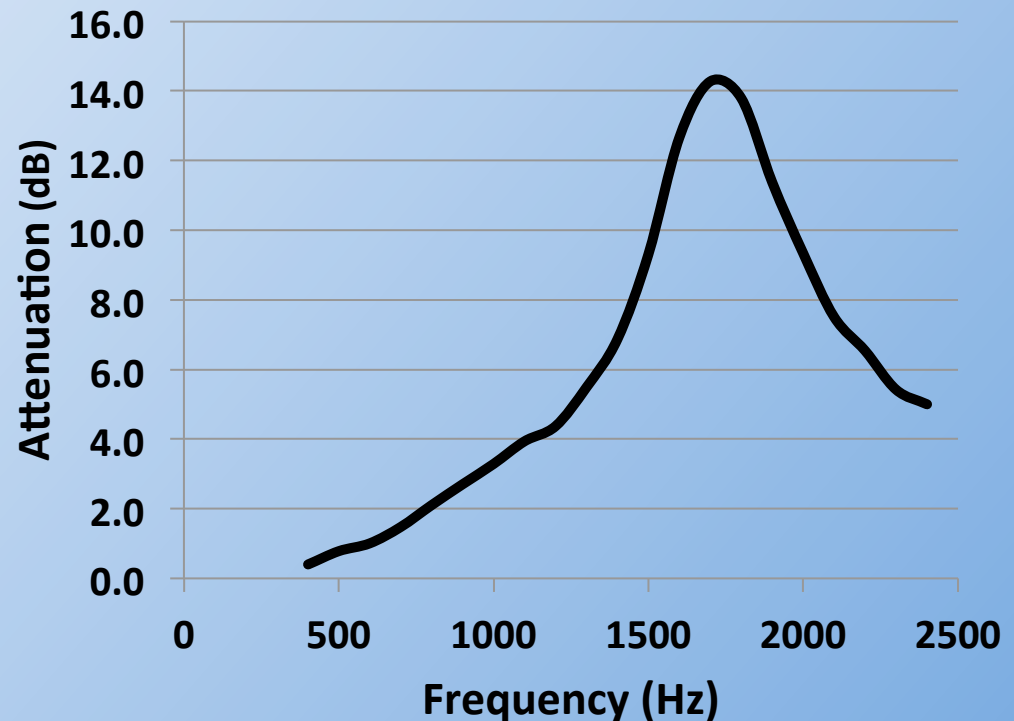


# SDOF Liner - Solid Back Plane

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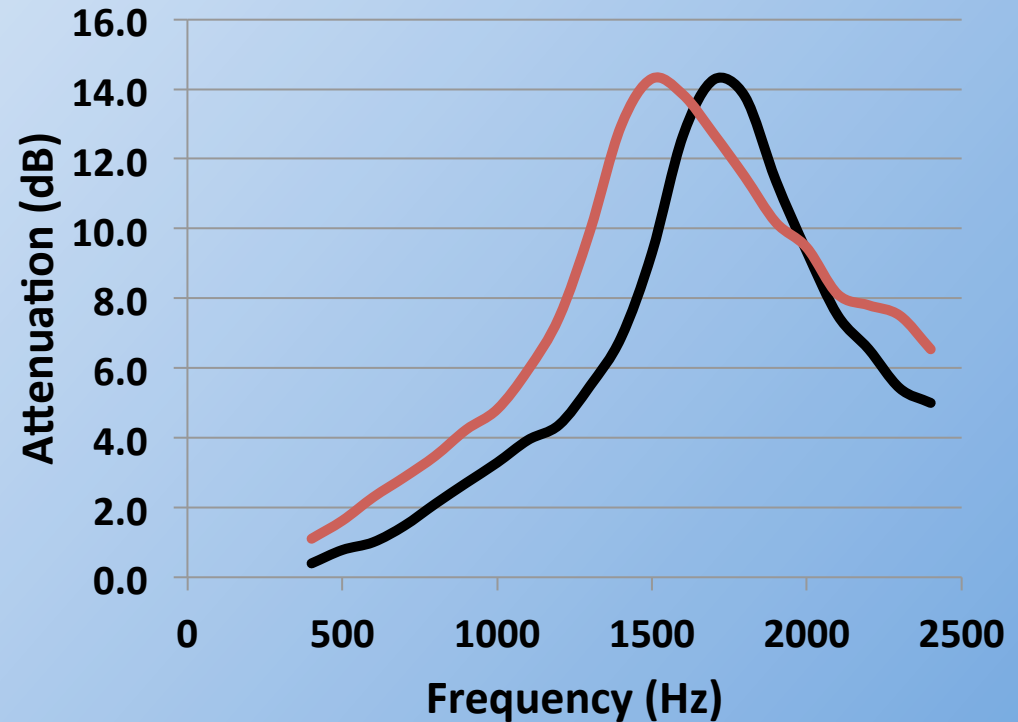
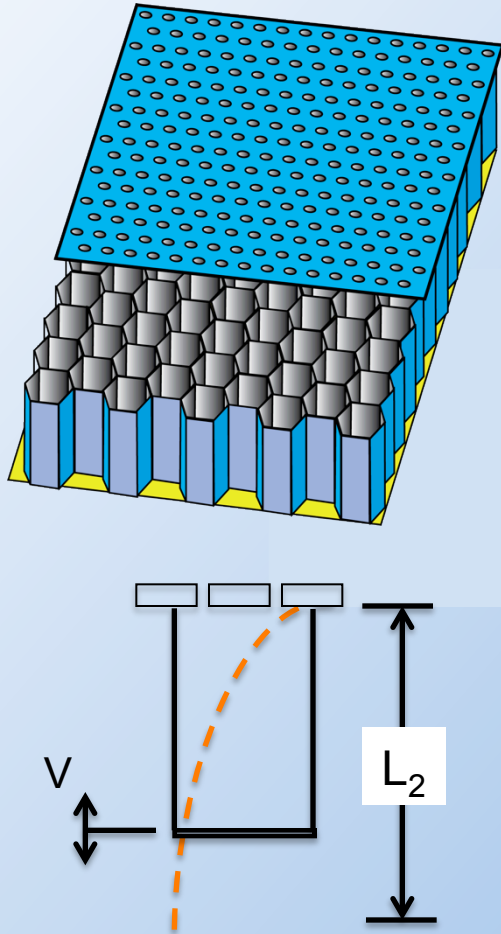
⇒ Frequency of peak attenuation fixed by  $L_1$





# Proposed Liner with Compliant Back Plane

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=> Compliant back plane can expand frequency range of attenuation



# Objectives of Research

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- Build samples coupons with piezo-electric material
- Determine acoustic and mechanical properties
- Estimate effect of material on liner attenuation





# Candidate Material

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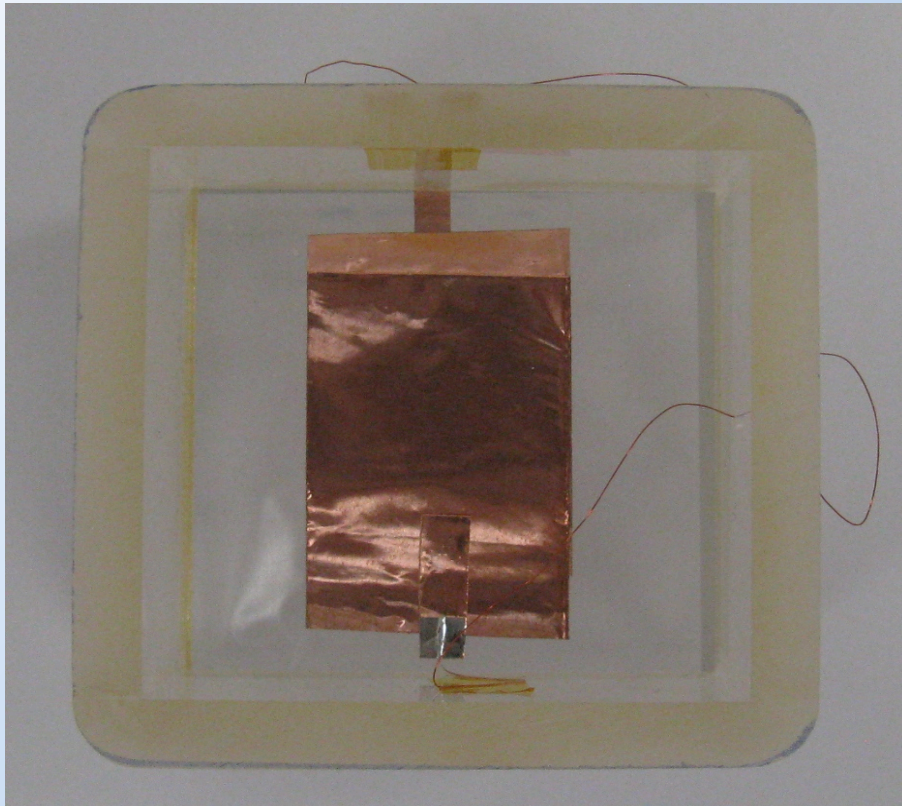
- PBLG Piezoelectric Composite Film
  - Composed of an  $\alpha$ -helical polypeptide
  - Produced via corona charging to pre-align macroscopic dipoles along helical axis
  - Responds to external force (sensor)
  - Responds to electric field (actuator)
  - Responds at acoustic frequencies
- Developed at Johns Hopkins University Applied Physics Laboratory



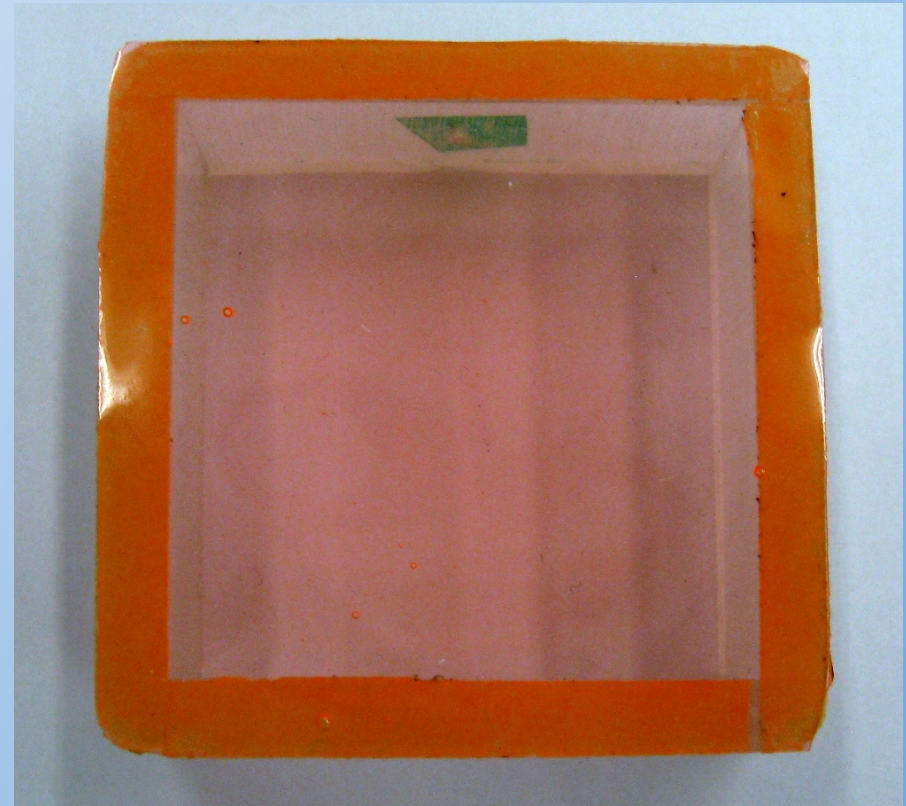
# Sample Coupons

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Unencapsulated sample with electrode



Encapsulated sample (without electrode)







# Samples Evaluated

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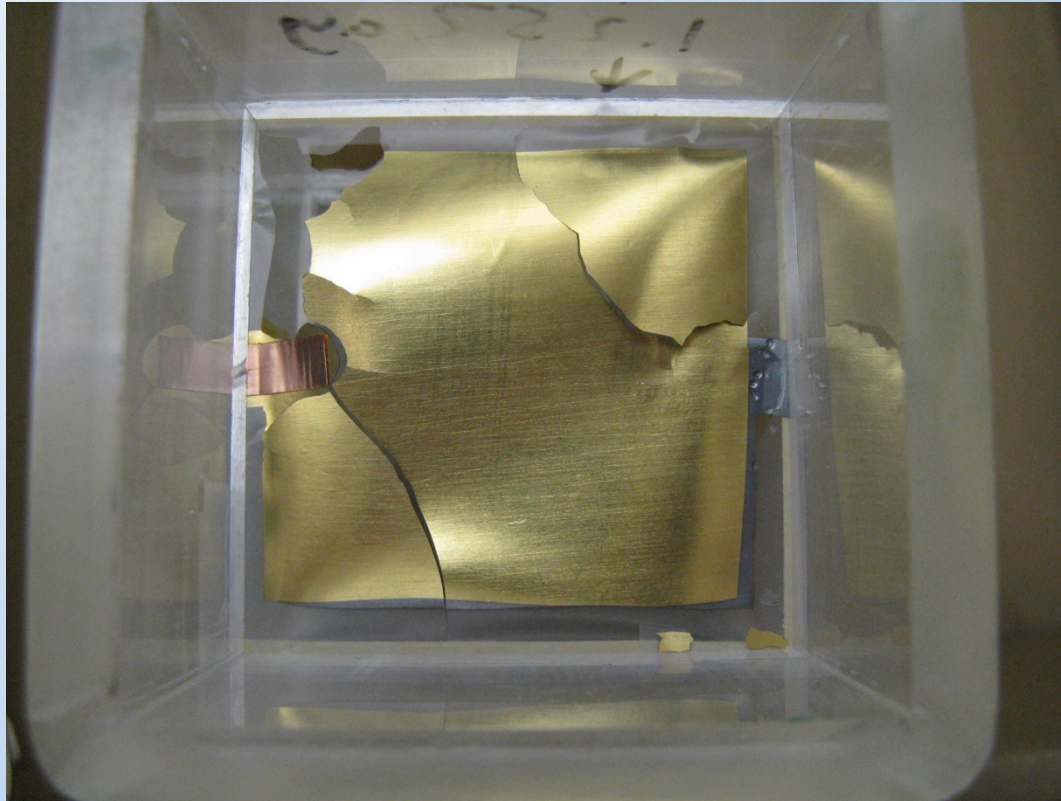
Sample	Description	Electrode	Electrode size	Status
JHS1	Composite film, no encapsulate	Cr-Au, evaporated	1"x1"	Functional
JHS2	Composite film, no encapsulate	Cr-Au, evaporated	1.75"x1.75"	Destroyed
JHS3	Composite film, encapsulated	No electrode	Na	Functional
JHS4	Composite film, no encapsulate	Conductive adhesive	1.75"x1.00"	Destroyed
JHS5	Composite film, encapsulated	No electrode	Na	Functional

**Table 1:** Cumulative list of samples received and the status from evaluating both standard un-encapsulated and encapsulated film samples.



# Sample JHS2 after Failure

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=> The un-encapsulated film was re-designed to offer samples with greater robustness



# Evaluate Properties

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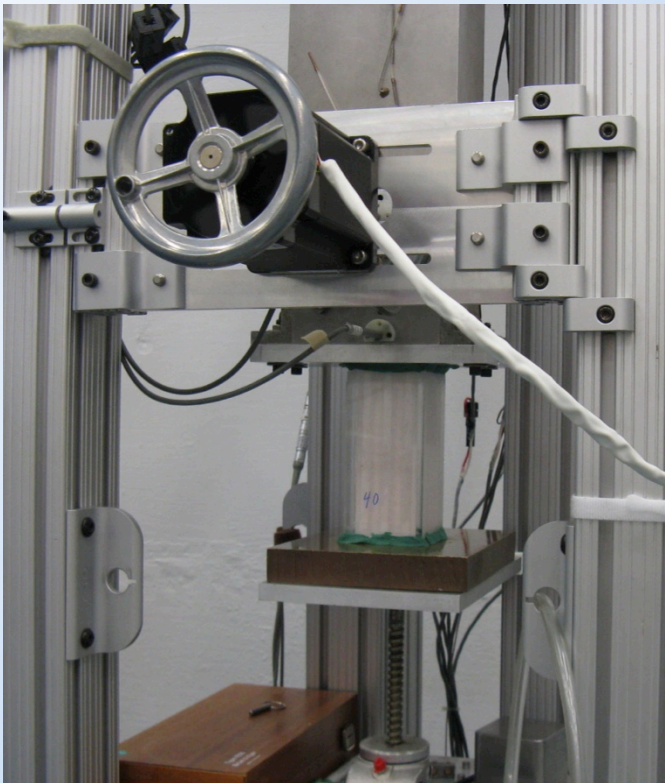
- Acoustic Properties
  - Measure acoustic impedance
  - Measure impedance change with voltage excitation
- Mechanical Properties
  - Measure velocity response to voltage excitation
  - Measure velocity response to acoustic excitation



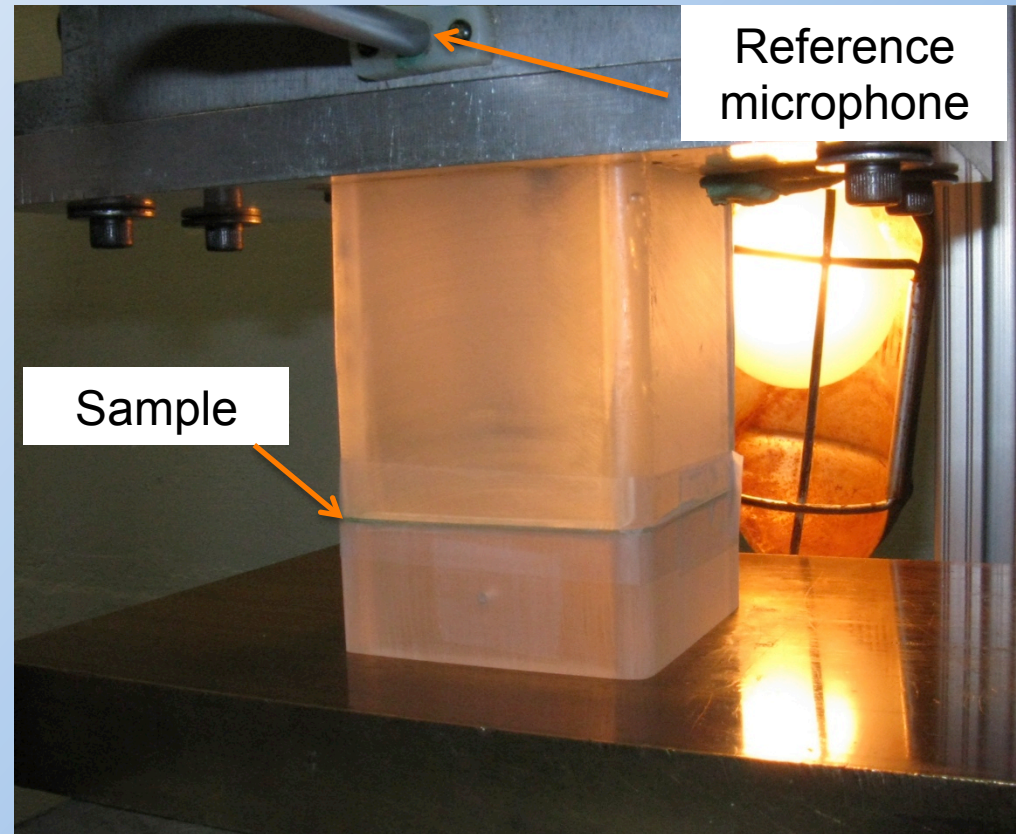


# Set-up for Normal Impedance Testing

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Normal Incidence Tube

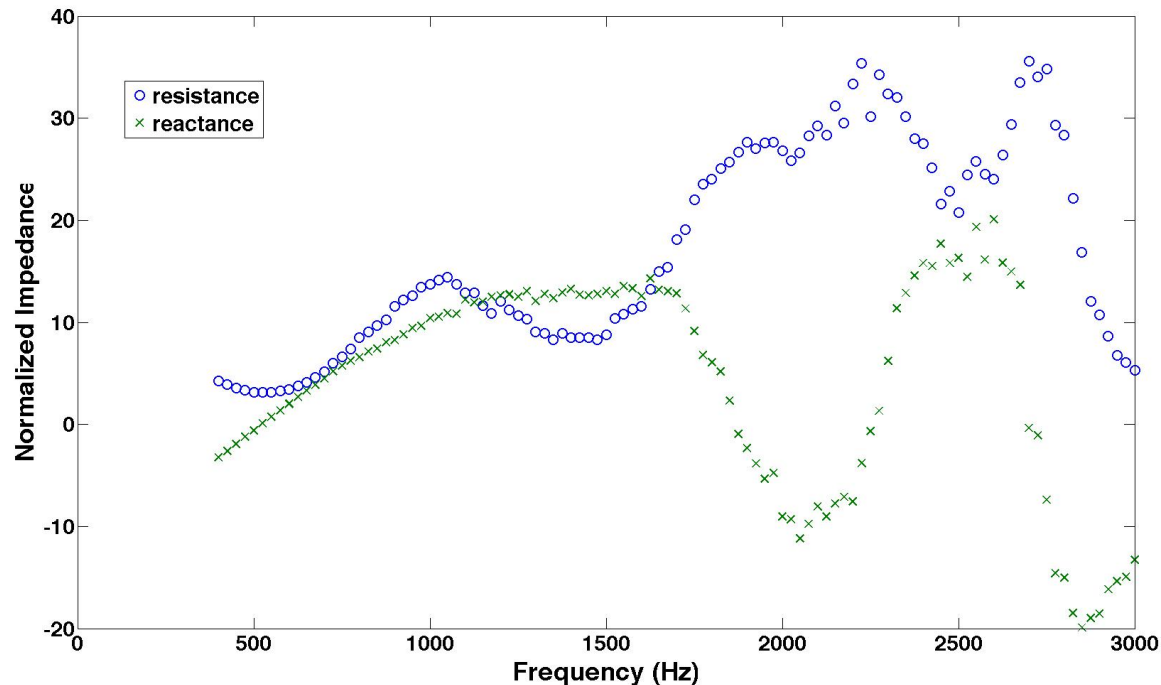


Piezo-electric sample in NIT



# Typical Impedance Measurement

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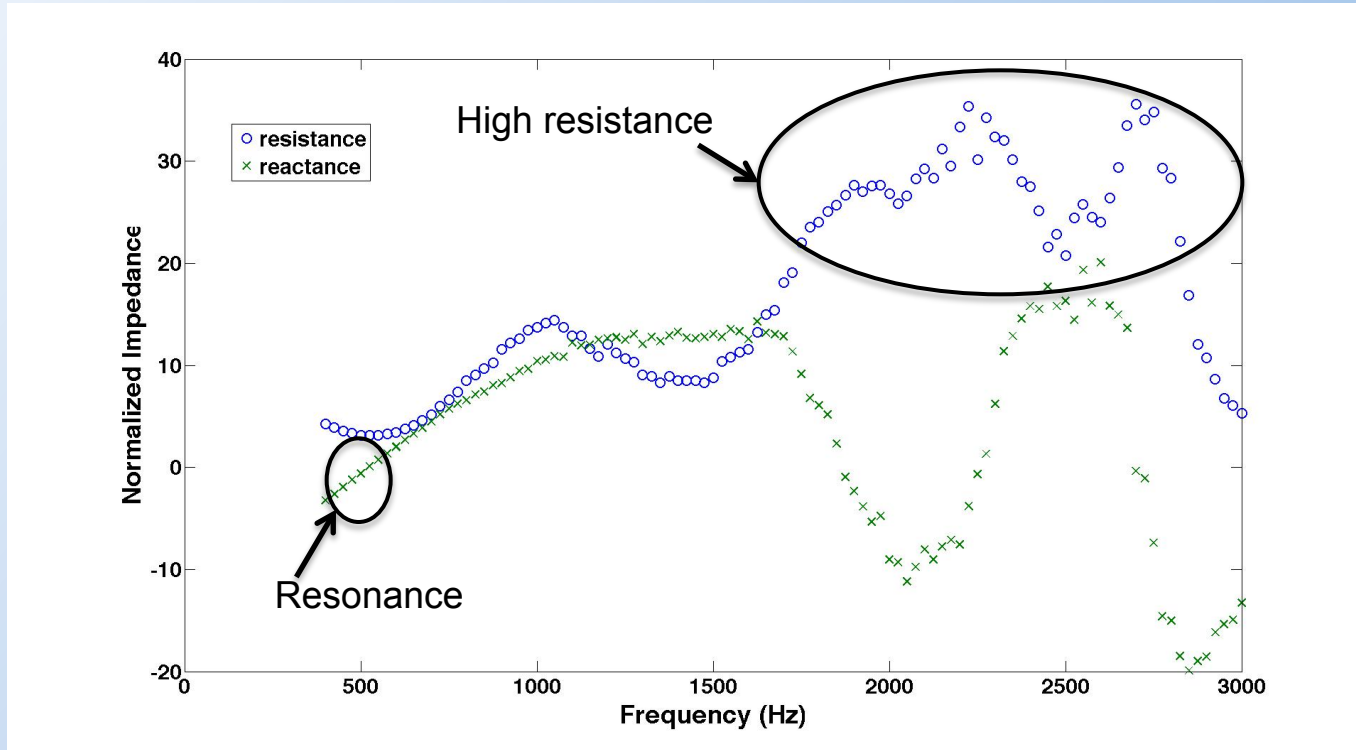
Impedance results from test set-up with encapsulated sample JHS3 evaluated with two-microphone method using broadband noise at 130 dB overall sound level.





# Typical Impedance Measurement

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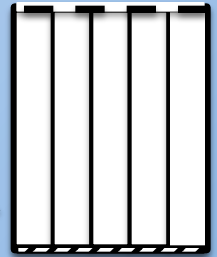
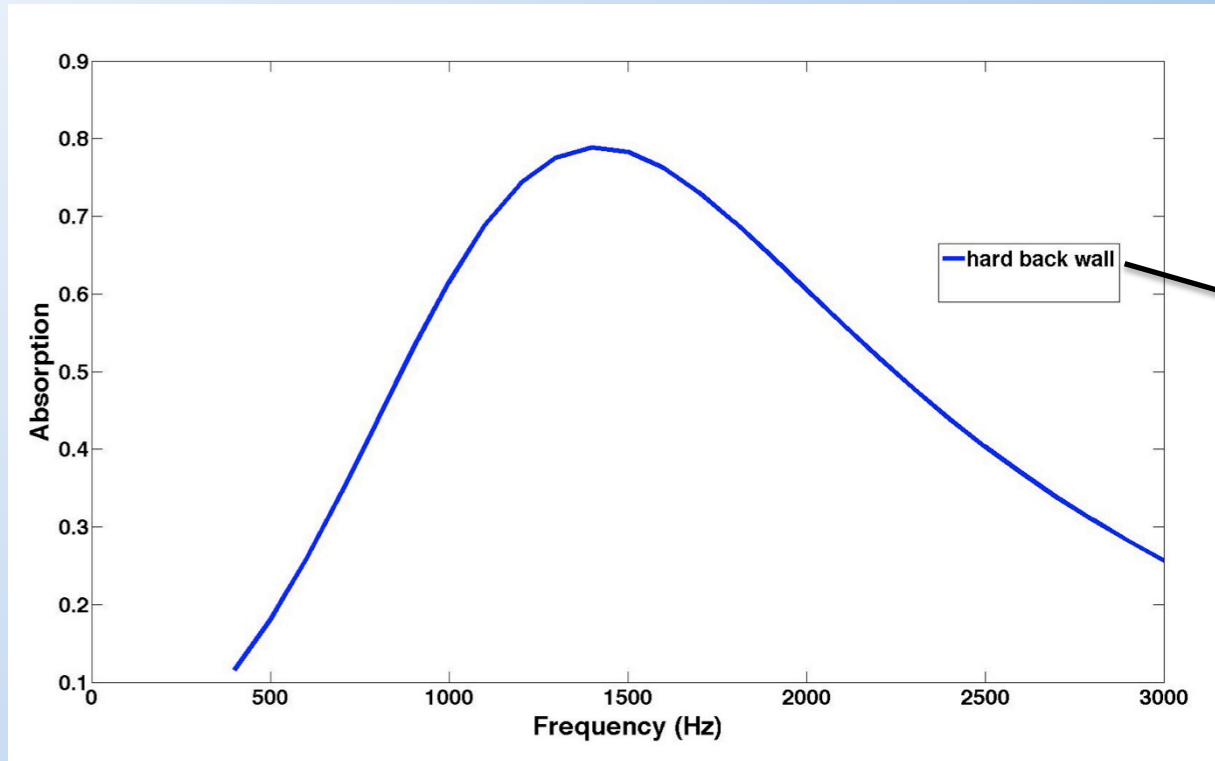


Impedance results from test set-up with encapsulated sample JHS3 evaluated with two-microphone method using broadband noise at 130 dB overall sound level.



# Application of Passive Compliant Back Wall

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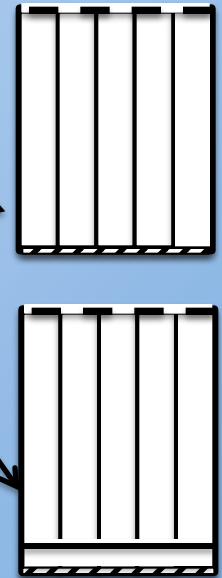
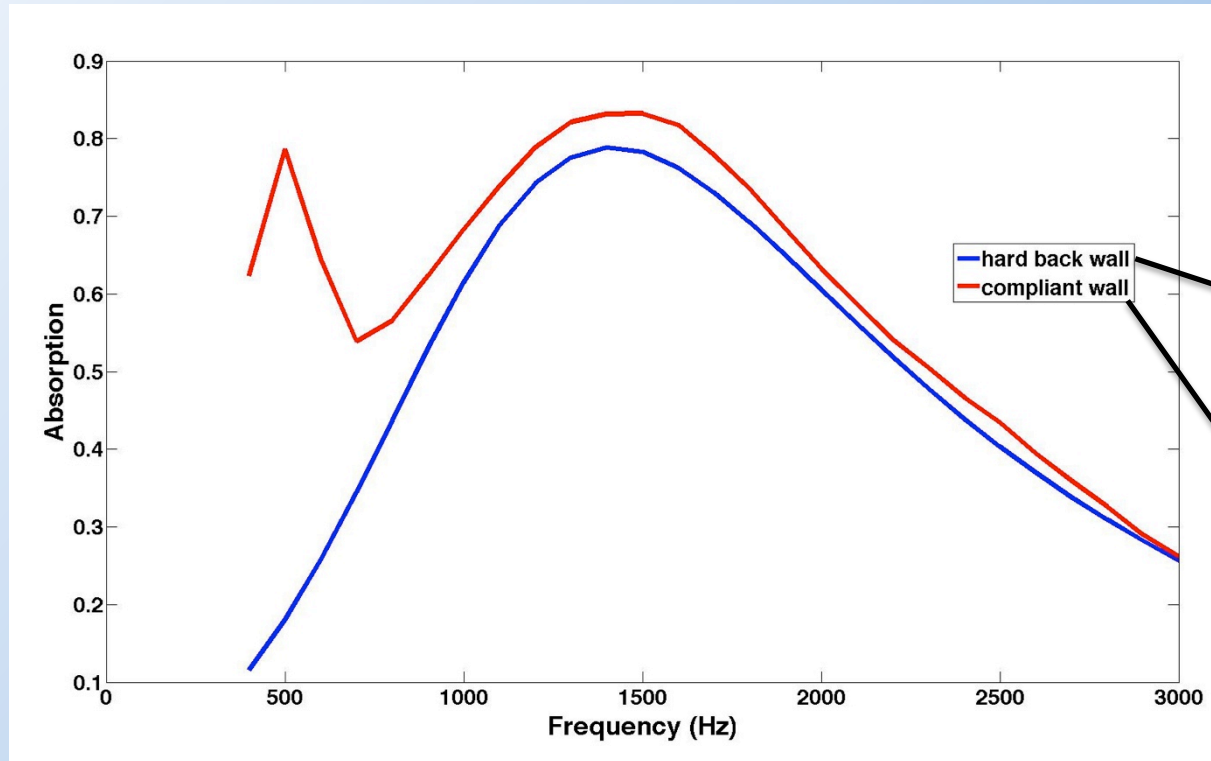


Calculated absorption of a perforate-over-honeycomb liner (core 1.50 in) compares rigid back wall to compliant back wall, JHS3.



# Application of Passive Compliant Back Wall

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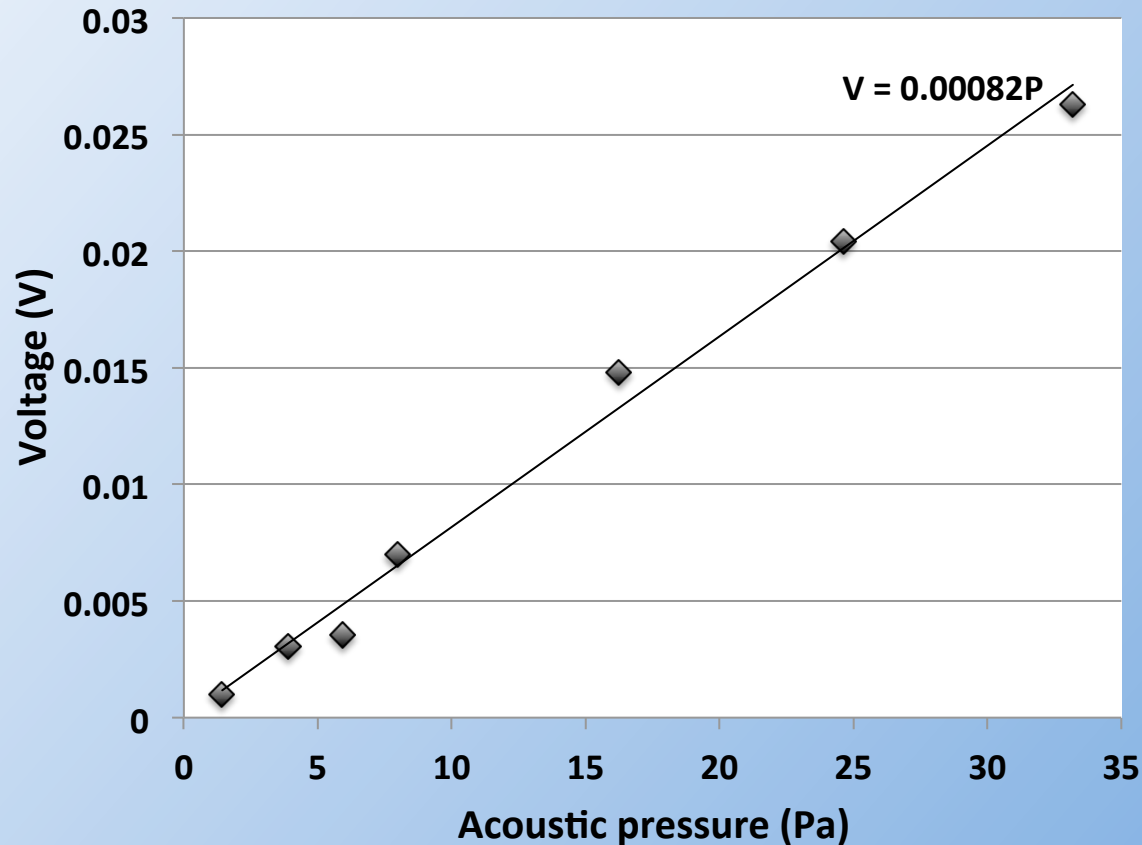
Calculated absorption of a perforate-over-honeycomb liner (core 1.50 in) compares rigid back wall to compliant back wall, JHS3.

=> Compliant back wall adds to liner absorption



# Piezoelectric Film as Sensor

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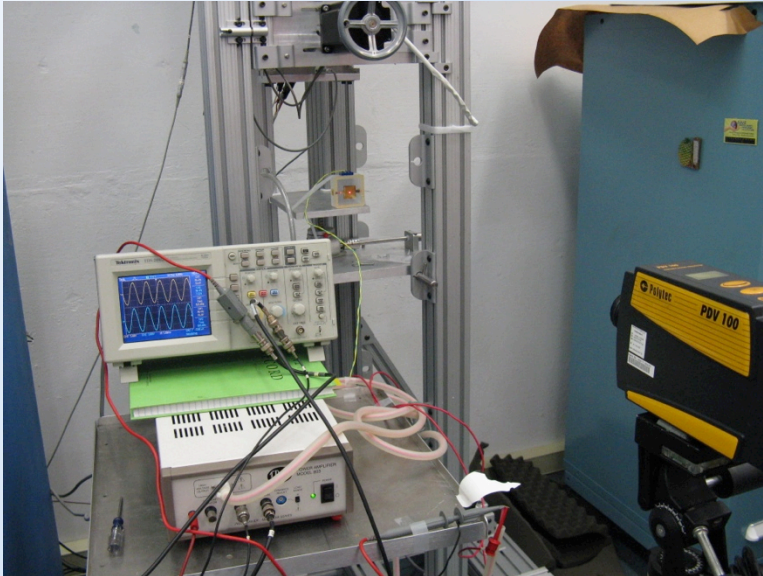


Voltage from electrode of sample JHS1 with acoustic excitation at 1000 Hz

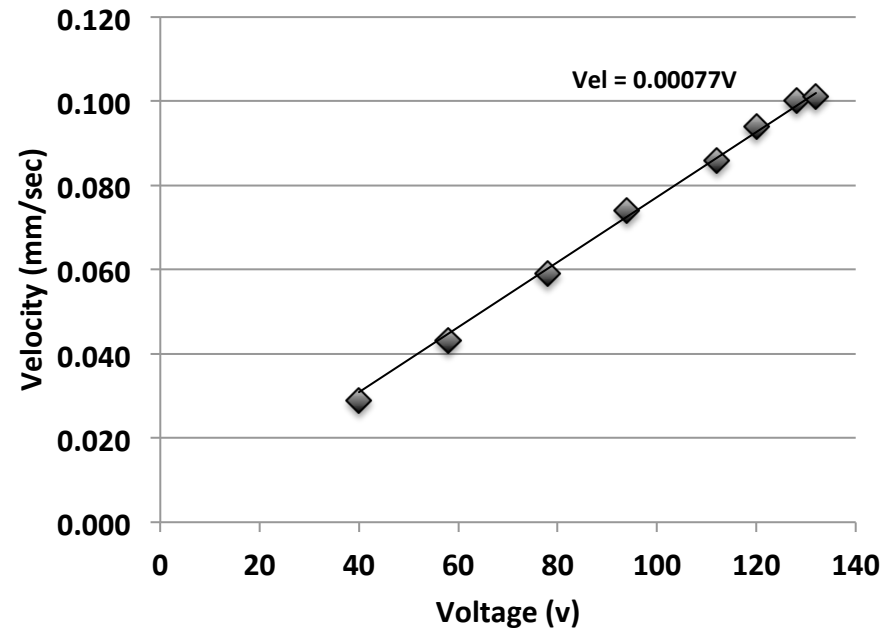


# Piezoelectric Film as Actuator

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Test set up for velocity measurement



Measured velocity of sample JHS1  
with voltage excitation at 1500 Hz

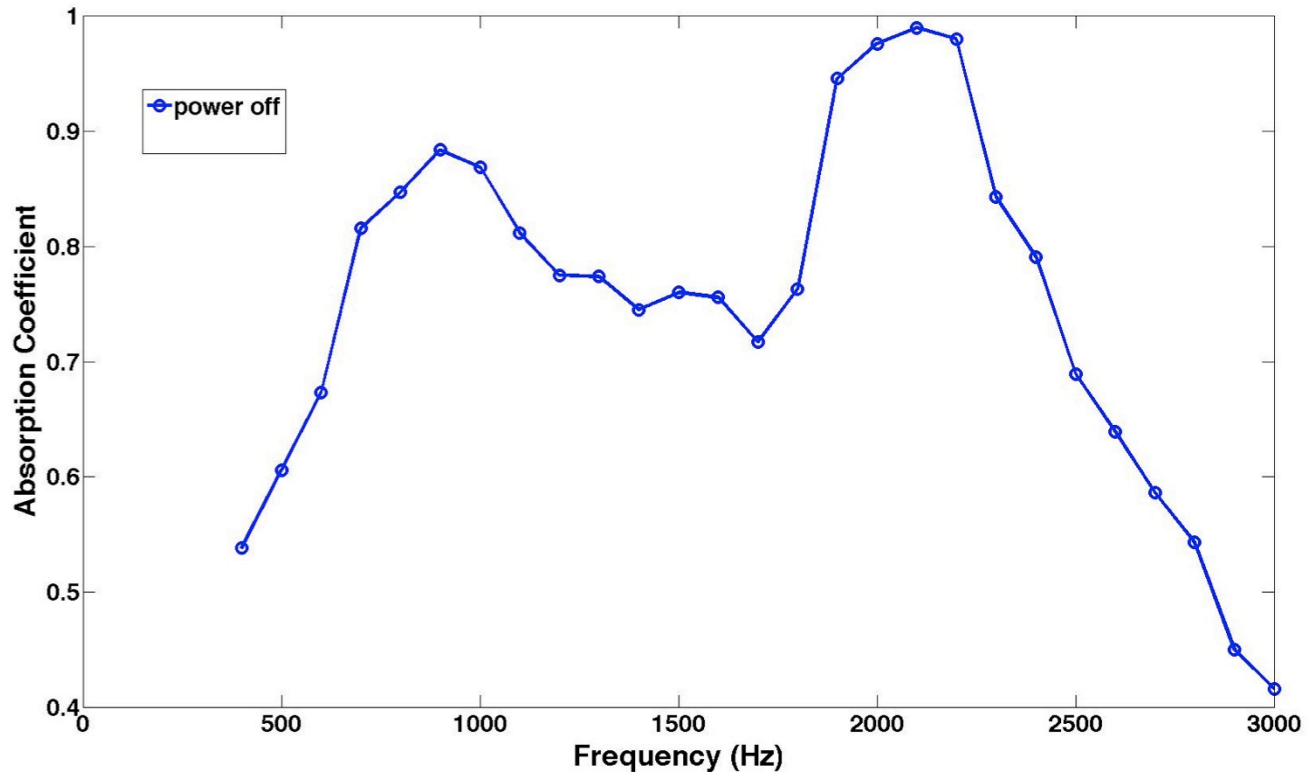
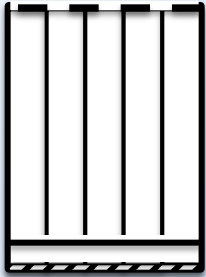
=> Velocity response much less than expected acoustic particle velocity





# Application of Active Compliant Back Wall

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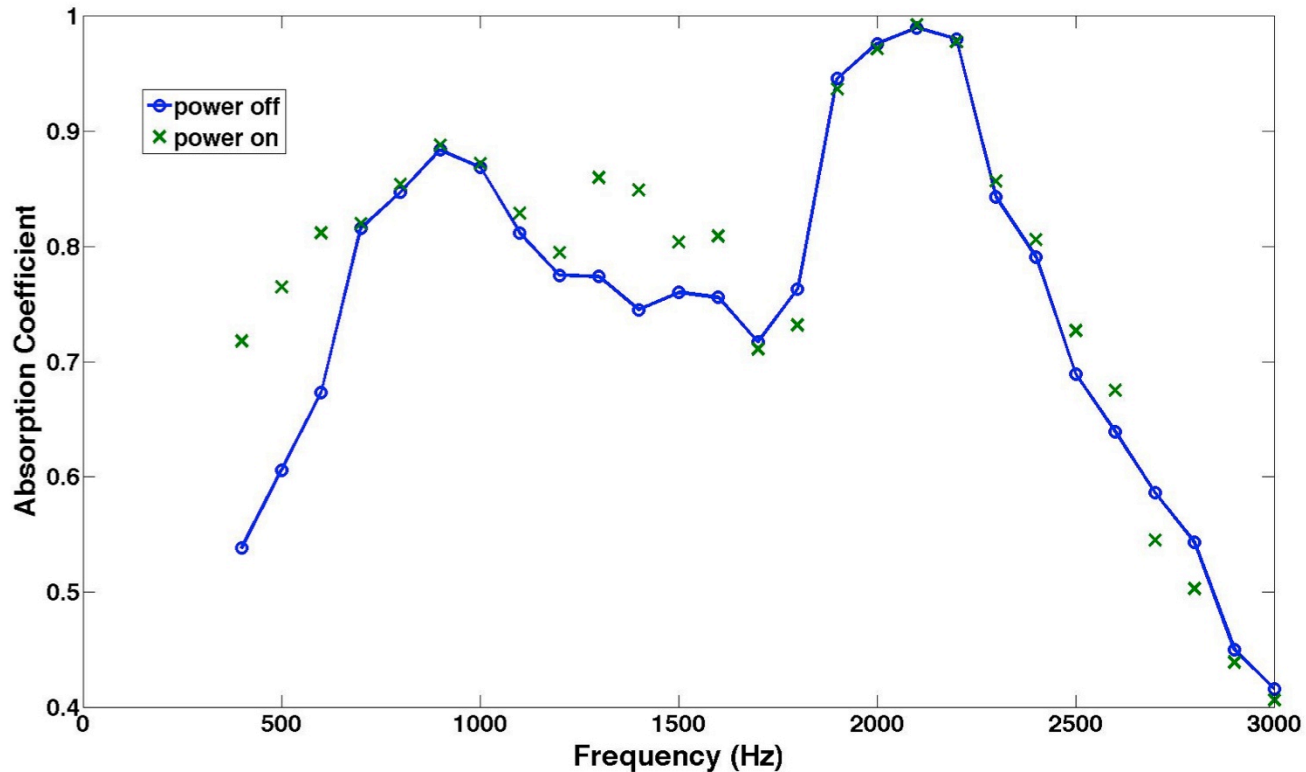
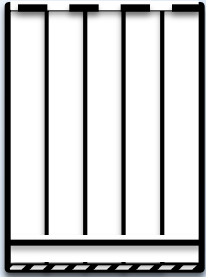


Calculated absorption coefficient of liner (core 1.5 in) with JHS1 backwall, compares power off to power on, 150 volt excitation



# Application of Active Compliant Back Wall

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Calculated absorption coefficient of liner (core 1.5 in) with JHS1 backwall, compares power off to power on, 150 volt excitation

=> Despite low authority, measurable change in liner absorption is indicated



# Conclusions (Part 1 of 2)

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- Developed liner samples for evaluation
  - Improved design to provide suitable robustness
- Developed experiments to evaluate the piezoelectric film samples
  - Measured mechanical properties
  - Measured acoustic properties



# Conclusions (Part 2 of 2)

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- Demonstrated that energizing the piezo-electric changes normal impedance in a controlled way
  - Current design lacks authority to alter impedance significantly.
- Developed mathematical model of liner absorption including compliant back wall
  - Model is semi-empirical



# Next Steps – Phase I

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- Incorporate piezoelectric into honeycomb structure
  - 2 in x 2 in sample for NIT
  - Estimate absorption of composite structure
  - Measure absorption to validate prediction
- Begin re-design of electrodes for greater authority
- Present results to date at Acoustics Technical Working Group
  - April 2013
  - October 2013





# Next Steps – Phase II

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- Improve electrode design
  - Increased authority
  - Incorporate in honeycomb structure
- Improve mathematical model of compliant wall effect
- Design, fabricate, and test active wall liner for Grazing Flow Impedance Tube
  - 2 inch x 24 inch liner sample size
  - Flow speed up to Mach 0.500
  - Tone and broadband sound input



# Thank You

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## **Adaptive Back Sheet Material for Acoustic Liner Application**